

**Lomonosov Moscow State University** 

Faculty of Mechanics and Mathematics

# Gas separation effect induced by filaments with different temperatures

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Development of new energy efficient methods for gas separation in membranes and microelectromechanical systems

Project



3. Transitional gas flow of mixture of gases in a region with moving boundaries and nonisothermal boundary conditions

#### Introduction





Membrane Knudsen pump as a gas separator



(S. Nakaye, H. Sugimoto, 2016)

and a large number of others...

0.009

 $p/\rho_{\rm ref}C_{\rm ref}^2$ 



(H. Sugimoto, S. Takata, S. Kosuge, 2007)

### **Separation device**

- Without movable elements
- Without temperature gradients in a solid
- Simple geometry







#### **Geometric parameters**



#### Problem statement



Initial mixture composition:  
(He, Ne, Ar, Kr, Xe)  
$$x_{0i} = 0.2$$

 $\bigcirc$  – Cold filament:  $T_w = T_0$ 

• – Hot filament: 
$$T_w = T_1 = 2T_0$$

#### Knudsen numbers:

 $Kn_L = \lambda/L = 0.1, 0.15, 0.2, 0.4$  $Kn_g = \lambda/g = 5, 10, 20, 40$   $\frac{\text{Geometries:}}{\frac{h}{d}} = 1.25, 1.5, 2, 3$ 

# 64 cases

#### Methods



#### **Event-driven Molecular Dynamics**



Trajectories of gas molecules between collisions – straight lines

- Intermolecular collisions,
- Collisions with solid surface,
- o ... other interactions in the simulation system

called "<mark>events</mark>"

RGD

RGD

The time in the simulation system is changed discretely – via times of events

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# Why EDMD?

Meshless – no mesh, no time step Fully deterministic – no adjustment parameters Without stochastic collision pair selection Without simplification of the collision integral

Our interest in the EDMD approach is caused by the possibility of its application to the problems of separation of multicomponent gas mixtures in devices with oscillating elements, because EDMD unlike the most of existing particle and mesh methods can be naturally generalized to the case of moving boundaries without significant complications of algorithm.





- Coordinates
- z Velocity
  - time when
    molecule obtained
    these coordinates
    and velocity

# Between collisions molecule moves along a straight line

$$\vec{x}(t) = \vec{x}' + \vec{v}'(t - t')$$

where  $\vec{x}'$  – coordinates of molecule after last collision,  $\vec{v}'$  – velocity of molecule after last collision, t' – time of last collision

#### Collisions with solid surface:

The time of *i*-th molecule collision with *k*-th boundary flat element can be found from linear equation:

$$\vec{x}_i(t) \cdot \vec{n}_k = R_k$$

Boundary element types:



flat element



cylinder

#### Hard spheres (HS) model was used:



The time of *i*-th and *j*-th molecules collision can be found from this quadratic equation

$$\left(\vec{x}_i(t) - \vec{x}_j(t)\right)^2 = \left(\frac{d_i}{2} + \frac{d_j}{2}\right)^2$$

### **Events**



Node event list

Event 1

Event 2

Event 3

Event 4

Event 5



Size of event list will be greater than number of molecules

#### Event-driven Molecular Dynamics



The most expensive operation during the simulation is search of place for insertion of new event!



#### Benchmark computation #1 – Flow in plane channel of finite length



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Relative statistical error of mass flow

$$e = \frac{\sigma}{a\sqrt{N}} = \frac{2}{N_{+} - N_{-}} \sqrt{\frac{N_{+}N_{-}}{N}} < 1\%$$

Supercomputer "Lomonosov" (based on Intel Xeon X5570 2.93GHz) Statement 1 – used less than 400MB RAM per core Statement 2 – used less than 1.3GB RAM per core Computation time = 50 hours

#### Benchmark computation #2 – Supersonic flow past cylinder





#### Benchmark computation #2 – Supersonic flow past cylinder



Before EDMD computation three parameters should be preset: hash-table parameters ( $\Delta_h$  and  $N_h$ ) and cell size c.

(result of simulation doesn't depend on these parameters – only speed of calculation)



$$\Delta_h = c \beta / \sqrt{\pi} N$$
$$\frac{c}{\delta} = \frac{1}{2}$$
$$\prod_{V}$$

The optimal number of cells should be approximately 8 times greater than the number of particles!

This confirms the result obtained in S. Miller, S. Luding, J. Comput. Phys. 193 (2004) 306–316.

y

Reservoir  $p_0, T_0, x_{0i}$ 



Equilibrium state with certain numerical density n, mean velocity  $\vec{\vartheta}$  and temperature T:

$$\rho(\vec{u}) = \frac{n}{J_1} \left(\frac{\beta}{\sqrt{\pi}}\right)^3 u_n exp\left(-\beta^2 \left(\vec{u} - \vec{\vartheta}\right)^2\right),$$
$$\eta_1 = n \left(\frac{\beta}{\sqrt{\pi}}\right)^3 \int_{0}^{\infty} \iint_{0}^{\infty} u_n exp\left(-\beta^2 \left(\vec{u} - \vec{\vartheta}\right)^2\right) d\vec{u} = 0$$

h

g

$$J_{1} = n \left(\frac{1}{\sqrt{\pi}}\right) \int_{0} \iint_{-\infty} u_{n} exp \left(-\beta^{2} \left(\vec{u} - \vartheta\right)\right) d\vec{u} = \frac{n}{2\sqrt{\pi}\beta} \left(exp(-\beta^{2}\vartheta_{n}^{2}) + \sqrt{\pi}\beta\vartheta_{n} erfc(-\beta\vartheta_{n})\right)$$

Solid wall and filaments surface

 $T_0$ 

х

Maxwell scattering kernel with full accommodation:

L

$$\rho(\vec{u}) = \frac{2\beta_w^4 u_n}{\pi} exp(-\beta_w^2 u^2),$$
$$\beta_w = \sqrt{m/2 kT_w}$$

Results

 $Kn_L = \lambda/L = 0.15$   $Kn_g = \lambda/g = 40$   $\frac{h}{d} = 1.25$ 

(case #13)



Separation takes place in chambers **between stages!** 

#### Qualitative physical explanation

Heat transfer between two walls -



#### Results

#### Xe molar concentration at the closed end of the system





$$---Kn = 0,1 ---Kn = 0,15 ---Kn = 0,2 ---Kn = 0,4$$

There is no sense in increasing the  $Kn_g \geq 20$  and decreasing the  $Kn_L \leq 0.2$ 



# Heat flux



 $\Box Kn_g=5 \Delta Kn_g=40$ 

 $Kn_L = 0.15$ 

$$Q_i^* = d_v \sqrt{\frac{2\pi kT_1}{m_i}} px_{0i} \left(1 - \left(\frac{T_2}{T_1}\right)^{\frac{3}{2}}\right) h_z$$

A plane problem about the transitional flow of a mixture of five noble gases in a system consisting of several rows of stretched filaments having different temperatures was studied.

It was obtained that separation takes place exactly in chambers between stages due to regular thermal diffusion, rather than inside stages.

It also means that **geometry of filaments doesn't play significant role in separation**. The main requirement is that flow between filaments has to be in near free-molecular regime, while flow in chambers has to be in near continual regime.

Also found that for  $Kn_g \ge 20$  and  $Kn_L \le 0.2$  further oncoming to the free-molecule limit inside stage and to the continuum limit between stages insignificantly increases the separation effect.

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## Thank you for attention!



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